# APPENDIX 10D Electrical Engineering Design Criteria

# **Electrical Engineering Design Criteria**

### 10D1 Introduction

This appendix summarizes the codes, standards, criteria, and practices that will be generally used in the design and construction of electrical engineering systems for the facility. More specific project information will be developed prior to construction of the project to support detailed design, engineering, material procurement, and construction specifications as required by the California Energy Commission (CEC).

### 10D2 Codes and Standards

The design of the electrical systems and components will be in accordance with the laws and regulations of the federal government, State of California and industry standards. The current issue or revision of the documents at the time of the filing of this Application for Certification (AFC) will apply, unless otherwise noted. If there are conflicts between the cited documents, the more conservative requirement shall apply.

The following codes and standards are applicable to the electrical aspects of the power facility.

- American National Standards Institute (ANSI)
- American Society for Testing and Materials (ASTM)
- Anti-Friction Bearing Manufacturers Association (AFBMA)
- Insulated Cable Engineers Association (ICEA)
- Institute of Electrical and Electronics Engineers (IEEE)
- Illuminating Engineering Society (IES)
- California Electrical Code (CEC)
- National Electrical Manufacturers Association (NEMA)
- National Electrical Safety Code (NESC)
- National Fire Protection Association (NFPA)
- Underwriters Laboratories, Inc. (UL)

## 10D3 Switchyard and Transformers

### 10D3.1 Switchyard

The switchyard will be located on the west end of the site and will interconnect to PG&E's nearby Potrero substation with aboveground aerial cables or with underground cables depending upon the final design interface with PG&E. The switchyard will be of the air-insulated aluminum bus type and will consist of high voltage SF<sub>6</sub>-insulated dead-tank circuit breakers arranged in a ring-bus configuration. Connections to the ring bus nodes will be provided for each generator and for the inter-ties to the utility grid. Each circuit breaker

will be equipped with a no load break, air-insulated, disconnect switch on each side. An isolating disconnect switch will also be installed in each generator transformer connection to the ring bus to allow continuous ring integrity when a transformer is out of service. Air-insulated tubular aluminum bus will be used as the primary bus construction and interconnection material within the switchyard. The buses will be attached to post insulator columns on structural steel supports.

Current and voltage transformers will be located at points within the switchyard to provide for metering and relaying.

Control, protection and monitoring for the switchyard will be located in the switchyard relay room of the electrical building. Monitoring and alarms will be available to the DCS operator workstations in the control room. All protection and circuit breaker control will be powered from the station battery-backed 125 Vdc system.

The switchyard design will meet the requirements of the National Electrical Safety Code – ANSI C2.

A grounding grid will be provided to control step and touch potentials in accordance with IEEE Standard 80, Safety in Substation Grounding. All equipment, structures and fencing will be connected to the grounding grid of buried copper conductors and ground rods, as required. The substation ground grid will be tied to the plant ground grid.

Lightning protection will be provided by shield wires and/or lightning masts for any overhead lines. The lightning protection system will be designed in accordance with IEEE 998 guidelines.

All faults shall be detected, isolated, and cleared in a safe and coordinated manner as soon as practical to insure the safety of Equipment, Personnel, and the Public. Protective relaying will meet IEEE requirements and will be coordinated with PG&E's requirements.

The ring bus will be provided with over-lapping high impedance differential relay systems. The protection will be designed to maintain ring bus integrity when isolating a faulted node. Each outgoing line to the utility substation 115-kV bus will be provided with redundant high-speed relay systems with transfer trip capability. Each circuit breaker will be provided with independent breaker failure relay protection scheme. Breaker failure protection will be accomplished by protective and timing relays for each breaker. Each high voltage breaker will have 2 redundant trip coils.

Interface with PG&E's supervisory control and data acquisition (SCADA) system will be provided. Interface will be at the interface terminal box and RTU. Communication between the facility switchyard and the control building to which it is connected will be included.

Revenue metering will be provided on the 115-kV outgoing lines recording net power to or from the PG&E switchyard (bi-directional). The revenue meters and a metering panel will be located in the switchyard relay room.

### 10D3.2 Transformers

Each generator will be connected to the 115kV switchyard through a separate 13.8-kV to 115-kV step-up transformer and a generator 15 kV metal-clad vacuum circuit breaker. The

step-up transformers will be designed in accordance with ANSI standards C57.12.00, C57.12.90, and C57.116. The transformers will be two-winding, delta-wye, ONAN/ONFA/ONAF, 65°C rise. The neutral point of the HV winding wye-connected winding will be solidly grounded. Each main step-up transformer will have metal oxide surge arrestors adjacent to the HV terminals and will have manual de-energized ("no-load") tap changers located in the HV windings.

Facility power will be supplied through unit auxiliary transformers connected to two of the 13.8-kV generator output busses. Two two-winding, delta-wye 13.8-kV to 4.16-kV transformers with low-impedance grounding resistors will be provided.